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# IN THE CLAIMS

(Currently Amended) An alloy composition comprising: 1.

titanium; and

a molybdenum equivalent weight of about 7 to about 11 wt%, wherein the weight percents are based upon the total weight of the alloy composition, wherein the alloy composition is superclastic and/or pseudoclastic, wherein the composition is devoid of niobium.

- (Original) The composition of Claim 1, wherein the composition is cold worked 2. and/or solution treated; and wherein the solution treating can be conducted at a temperature above and/or below the  $\beta$  transus temperature.
- (Original) The composition of Claim 1, wherein the molybdenum equivalent weight is determined by the equation (1)

$$Mo_{eq.} = 1.00Mo + 0.28Nb + 0.22Ta + 0.67V + 1.43Co + 1.60Cr + 0.77Cu + 2.90Fe + 1.54Mn + 1.11Ni + 0.44W - 1.00Al$$
 (1)

or the equation (2)

$$Mo_{eq.} = 1.00Mo + 0.28Nb + 0.22Ta + 0.67V + 1.43Co + 1.60Cr + 0.77Cu + 2.90Fe + 1.54Mn + 1.11Ni + 0.44W + 0.25(Sn + Zr + Hf) - 1.00Al$$
 (2)

wherein Mo is molybdenum, Nb is niobium, Ta is tantalum, V is vanadium, Co is cobalt, Cr is chromium, Cu is copper, Fe is iron, Mn is manganese, Ni is nickel, W is tungsten, Al is aluminum, Sn is tin, Zr is zirconium and Hf is hafnium; wherein aluminum can be substituted by gallium, carbon, germanium and/or boron; and wherein the respective chemical symbols represent the amounts of the respective elements in weight percent based on the total weight of the alloy composition.

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(Currently Amended) The composition of Claim 1, comprising: 4.

about 8 to about 10-9.75 wt% molybdenum,

about 2.8 to about 6 wt% aluminum,

up to about 2 wt% vanadium,

up to about 4 wt% niobium, with the balance being titanium, wherein the weight percents are based on the total weight of the alloy composition, and wherein the composition is cold worked.

- (Original) The composition of Claim 4, further comprising solution treating the 5. composition at a temperature of greater than or equal to the  $\beta$  transus temperature for a time period of greater than or equal to about 30 seconds.
- 6. (Original) The composition of Claim 5, wherein the temperature is about 850 to about 1000°C.
- (Original) The composition of Claim 4, further comprising solution treating the 7. composition at a temperature of less than or equal to the  $\beta$  transus temperature for a time period of greater than or equal to about 1 minute.
- (Original) The composition of Claim 7, wherein the temperature is about 750 to 8. about 850°C.
- (Original) The composition of Claim 1, wherein the composition has a  $\beta$  phase 9. and/or an  $\alpha$  and a  $\beta$  phase.
- (Original) The composition of Claim 1, wherein the composition has an elastic recovery of greater than or equal to about 75% of the applied change in length when the applied change in length is 2% of the original length.

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- 11. (Original) The composition of Claim 1, wherein the composition has an elastic recovery of greater than or equal to about 85% of the applied change in length when the applied change in length is 2% of the original length.
- 12. (Original) The composition of Claim 1, wherein the composition has an elastic recovery of greater than or equal to about 50% of the applied change in length when the applied change in length is 4% of the original length.
- 13. (Original) The composition of Claim 1, wherein the composition has an elastic recovery of greater than or equal to about 75% of the applied change in length when the applied change in length is 4% of the original length.
- 14. (Original) The composition of Claim 1, wherein the composition after cold working has a reduction in the elastic modulus of greater than or equal to about 10% when compared with the elastic modulus of an equivalent heat treated composition.
- 15. (Original) The composition of Claim 1, wherein the composition after cold working has a reduction in the elastic modulus of greater than or equal to about 20% when compared with the elastic modulus of an equivalent heat treated composition.
- 16. (Original) The composition of Claim 1, wherein the composition after cold working has a reduction in the elastic modulus of greater than or equal to about 25% when compared with the elastic modulus of an equivalent heat treated composition.
- 17. (Original) The composition of Claim 4, wherein the composition, after cold working and/or solution treating, has an elastic recovery of greater than or equal to about 75% of the applied change in length when the applied change in length is 2% of the original length.

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18. (Original) The composition of Claim 4, wherein the composition, after cold working and/or solution treating, has an elastic recovery of greater than or equal to about 85% of the applied change in length when the applied change in length is 2% of the original length.

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- (Original) The composition of Claim 4, wherein the composition, after cold 19. working and/or solution treating, has an elastic recovery of greater than or equal to about 50% of the applied change in length when the applied change in length is 4% of the original length,
- (Original) The composition of Claim 4, wherein the composition, after cold 20. working and/or solution treating, has an elastic recovery of greater than or equal to about 75% of the applied change in length when the applied change in length is 4% of the original length.
- (Original) The composition of Claim 4, wherein the composition, after cold 21. working, has a reduction in the elastic modulus of greater than or equal to about 10% when compared with the elastic modulus of an equivalent heat treated composition.
- (Original) The composition of Claim 4, wherein the composition, after cold 22. working, has a reduction in the elastic modulus of greater than or equal to about 20% when compared with the elastic modulus of an equivalent heat treated composition.
- (Original) The composition of Claim 4, wherein the composition, after cold 23. working, has a reduction in the elastic modulus of greater than or equal to about 25% when compared with the elastic modulus of an equivalent heat treated composition.
  - 24. (Original) An article manufactured from the composition of Claim 1.
  - (Original) An article manufactured from the composition of Claim 4. 25,

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# 26. (Withdrawn) A method for making an article comprising:

working a shape, wherein the shape has a composition comprising titanium; and a molybdenum equivalent weight of about 7 to about 11 wt%, wherein the weight percents are based upon the total weight of the alloy composition; and wherein the molybdenum equivalent weights are determined by the equation (1)

$$Mo_{eq.} = 1.00Mo + 0.28Nb + 0.22Ta + 0.67V + 1.43Co + 1.60Cr + 0.77Cu + 2.90Fe + 1.54Mn + 1.11Ni + 0.44W - 1.00Al$$
 (1)

or the equation (2)

$$Mo_{eq.} = 1.00Mo + 0.28Nb + 0.22Ta + 0.67V + 1.43Co + 1.60Cr + 0.77Cu + 2.90Fe + 1.54Mn + 1.11Ni + 0.44W + 0.25(Sn + Zr + Hf) - 1.00Al$$
 (2)

wherein Mo is molybdenum, Nb is niobium, Ta is tantalum, V is vanadium, Co is cobalt, Cr is chromium, Cu is copper, Fe is iron, Mn is manganese, Ni is nickel, W is tungsten, Al is aluminum, Sn is tin, Zr is zirconium and Hf is hafnium; wherein the aluminum can be substituted by boron, carbon, gallium and/or germanium and wherein the respective chemical symbols represent the amounts of the respective elements in weight percent based on the total weight of the alloy composition;

solution treating the shape; and

cooling the shape.

- 27. (Withdrawn) The method of Claim 26, wherein the working is accomplished through cold working or hot working.
- 28. (Withdrawn) The method of Claim 26, wherein the solution treating is conducted at a temperature below the  $\beta$  transus temperature for the composition.
- 29. (Withdrawn) The method of Claim 26, wherein the solution treating is conducted at a temperature above the  $\beta$  transus temperature for the composition.

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- 30. (Withdrawn) The method of Claim 26, wherein the cooling is conducted in air and/or an inert gas.
- (Withdrawn) The method of Claim 26, wherein the shape is further heat aged at a 31. temperature of about 350 to about 550°C.
- (Withdrawn) The method of Claim 31, wherein the heat ageing is conducted for a 32. time period of 10 seconds to about 8 hours.
  - (Withdrawn) The method of Claim 26, further comprising cold working the shape. 33.
  - (Withdrawn) A method for making an article comprising: 34.

cold working a shape from a composition comprising about 8 to about 10 wt% molybdenum, about 2.8 to about 6 wt% aluminum, up to about 2 wt% vanadium, up to about 4 wt% niobium, with the balance being titanium, wherein the weight percents are based on the total weight of the alloy composition;

solution treating the shape; and

cooling the shape.

- (Withdrawn) The method of Claim 34, wherein the solution treating is conducted 35. at a temperature below the isomorphic temperature for the composition.
- (Withdrawn) The method of Claim 34, wherein the solution treating is conducted 36. at a temperature above the isomorphic temperature for the composition.
  - (Withdrawn) The method of Claim 34, wherein the cooling is conducted in air. 37.
- (Withdrawn) The method of Claim 34, wherein the shape is further heat aged at a 38. temperature of about 350 to about 550°C.
- (Withdrawn) The method of Claim 38, wherein the heat ageing is conducted for a 39. time period of 10 seconds to about 8 hours.

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- (Withdrawn) The method of Claim 34, further comprising cold working the shape. 40.
- (Withdrawn) A method comprising: 41.

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cold working a wire having a composition comprising titanium; and a molybdenum equivalent weight of about 7 to about 11 wt%, wherein the weight percents are based upon the total weight of the alloy composition; and wherein the molybdenum equivalent weights are determined by the equation (1)

$$Mo_{eq.} = 1.00Mo + 0.28Nb + 0.22Ta + 0.67V + 1.43Co + 1.60Cr + 0.77Cu + 2.90Fe + 1.54Mn + 1.11Ni + 0.44W - 1.00Al$$
 (1)

or the equation (2)

$$Mo_{eq.} = 1.00Mo + 0.28Nb + 0.22Ta + 0.67V + 1.43Co + 1.60Cr + 0.77Cu + 2.90Fe + 1.54Mn + 1.11Ni + 0.44W + 0.25(Sn + Zr + Hf) - 1.00Al$$
 (2)

wherein Mo is molybdenum, Nb is niobium, Ta is tantalum, V is vanadium, Co is cobalt, Cr is chromium, Cu is copper, Fe is iron, Mn is manganese, Ni is nickel, W is tungsten, Al is aluminum, S is tin, Zr is zirconium and Hf is hafnium; and wherein the respective chemical symbols represent the amounts of the respective elements in weight percent based on the total weight of the alloy composition;

solution treating the wire; and

heat treating the wire.

- (Withdrawn) The method of Claim 41, wherein the composition comprises about 8 42. to about 10 wt% molybdenum, about 2.8 to about 6 wt% aluminum, up to about 2 wt% vanadium, up to about 4 wt% niobium, with the balance being titanium, wherein the weight percents are based on the total weight of the alloy composition.
- (Withdrawn)The method of Claim 41, wherein the cold working results in a 43. reduction in cross-sectional area of about 5 to about 85%.

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(Withdrawn) The method of Claim 41, wherein the wire diameter is about 0.1 to 44. about 10 millimeters.

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- (Withdrawn) The method of Claim 41, wherein the heat treating is conducted at a 45. temperature of about 500°C to about 900°C.
  - (Withdrawn) The method of Claim 41, wherein the wire is solution treated at a 46. temperature of about 800 to about 1000°C.
- (Withdrawn) The method of Claim 41, wherein the article has a  $\beta$  phase or an  $\alpha$ 47. phase and a  $\beta$  phase.
- (Withdrawn) The method of Claim 41, wherein the article has an elastic recovery 48. of greater than or equal to about 75% of the applied change in length when the applied change in length is 2% of the original length.
- (Withdrawn) The method of Claim 41, wherein the article has an elastic 49. recovery of greater than or equal to about 50% of the applied change in length when the applied change in length is 4% of the original length.